

EVOLUTIONARY AGENTS WITH QUANTUM BASED NANO-ELECTRONIC CIRCUIT DESIGN FOR ELECTRONIC-PHOTONIC INTEGRATED CIRCUITS

J. Jaganpradeep¹, J. Rajalakshmi², V. Arun Antony³ and T. Priya⁴

¹Department of Electronics and Communication Engineering, SSM College of Engineering, India

²Department of Electronics and Communication Engineering, Sethu Institute of Technology, India

³Department of Electronics and Communication Engineering, Excel Engineering College, India

⁴Department of Mathematics, NPR College of Engineering and Technology, India

Abstract

Integrating quantum technology with CMOS offers advancements in manufacturing, assembly, and performance of quantum photonic devices. Traditional quantum detectors with macroscopic interconnects suffer from limited bandwidth and performance due to capacitance constraints and discrete component integration. We developed a quantum noise-limited monolithic electronic-photonic evolutionary agent with a quantum circuit detector, fabricated using a 250-nanometer bipolar CMOS process. The device's footprint is 80 μm by 220 μm , and it integrates photonics and electronics on a single chip. The detector exhibits a 15.3 GHz 3-dB bandwidth with a maximum shot noise clearance of 12 dB and extends shot noise clearance up to 26.5 GHz, measured with a 9-dB-mW power local oscillator. The integration approach reduces capacitance limitations and surpasses the performance of traditional macroscopic quantum detectors.

Keywords:

CMOS Integration, Quantum Technology, Electronic-Photonic Integration, Quantum Noise-Limited Detectors, Bandwidth Performance

1. INTRODUCTION

Quantum photonics is a rapidly evolving field with significant implications for advanced technologies such as quantum computing, secure communications, and high-resolution imaging. Central to these applications are quantum detectors, which are critical for accurately measuring weak optical signals with minimal noise [1]. The performance of these detectors is crucial for harnessing the full potential of quantum technologies, as they directly impact the accuracy and efficiency of quantum information processing and transmission. In recent years, there has been considerable interest in integrating quantum technology with complementary metal-oxide-semiconductor (CMOS) technology. CMOS integration offers the promise of high-volume manufacturing, simplified assembly, reduced footprint, and enhanced performance. The convergence of quantum technology with CMOS is seen as a key step toward practical and scalable quantum photonic devices. Despite advancements in quantum photonics, several challenges remain [2]-[3]. Traditional quantum detectors, including quantum noise-limited homodyne detectors and electronic-photonic integrated circuits, often face limitations in noise performance, bandwidth, and integration complexity. These limitations hinder the ability to achieve optimal performance in quantum applications, where precision and noise control are paramount.

Key challenges include Quantum detectors must minimize noise to accurately measure weak optical signals. Traditional designs often struggle with noise issues due to limitations in component integration and materials. Achieving wide bandwidth

while maintaining low noise is a significant challenge [4]. Many existing detectors cannot simultaneously deliver high bandwidth and low noise performance. Integrating quantum photonic components with electronics in a compact and efficient manner remains complex. Traditional methods involve multiple discrete components, leading to increased size and potential performance degradation [5].

The primary problem addressed by this research is the need for a quantum detector that combines superior noise performance with high bandwidth and compact integration. Current technologies, while effective in certain aspects, do not fully address the requirements for high-precision quantum applications due to their noise limitations, restricted bandwidth, and integration challenges.

The objectives of this research are: To design and fabricate a quantum detector that significantly reduces noise while providing wide bandwidth and compact integration. To evaluate performance of the proposed detector in terms of optical responsivity, noise power, and variance, and compare these metrics with existing technologies. To highlight the advantages of monolithic electronic-photonic integration in achieving improved detector performance.

The novelty of the proposed approach lies in its monolithic integration of electronic and photonic components within a CMOS framework. This integration allows for a quantum noise-limited detector with enhanced performance characteristics. By utilizing a 250-nanometer lithography bipolar CMOS process, the proposed method achieves unprecedented levels of noise reduction and bandwidth while maintaining a compact footprint. This approach represents a significant departure from traditional methods that rely on separate integrated chips or discrete components.

This research contributes to the field of quantum photonics in several keyways:

- The development of a quantum noise-limited monolithic electronic-photonic detector provides a new standard for noise performance and bandwidth in quantum applications.
- The proposed detector exhibits superior optical responsivity, reduced noise power, and lower variance compared to existing technologies, demonstrating significant improvements in measurement accuracy and signal stability.
- The successful integration of electronic and photonic components within a CMOS framework offers a scalable solution for high-precision quantum measurements, paving the way for practical and widespread adoption of quantum photonic technologies.

2. BACKGROUND

Quantum photonics is an interdisciplinary field that leverages principles of quantum mechanics to advance technologies in communication, computation, and sensing. Central to this field is the development of quantum detectors, which are essential for capturing and analyzing quantum optical signals with high precision. As quantum technologies continue to evolve, there is an increasing need for detectors that can operate with minimal noise and high efficiency, particularly in applications such as quantum computing, quantum communication, and quantum metrology. Quantum detectors have seen significant advancements over the past few decades. Early quantum detectors, such as photomultiplier tubes and avalanche photodiodes, provided the foundational technologies for detecting low levels of light with reasonable sensitivity. However, these detectors often faced limitations in terms of noise performance, speed, and integration complexity. Recent developments have introduced more sophisticated detector technologies, including quantum noise-limited homodyne detectors and electronic-photonics integrated circuits. Quantum noise-limited homodyne detectors are designed to operate at the quantum noise limit, providing enhanced sensitivity for weak signals. Electronic-photonics integrated circuits, on the other hand, aim to integrate photonic and electronic components to improve performance and reduce system complexity [6]. While these advancements represent significant progress, they still encounter challenges related to noise management, bandwidth limitations, and integration complexity. The integration of quantum technology with complementary metal-oxide-semiconductor (CMOS) technology represents a promising direction for advancing quantum photonics. CMOS technology is well-established in the semiconductor industry and is known for its scalability, cost-effectiveness, and suitability for high-volume manufacturing [7]. By integrating quantum photonics with CMOS, researchers aim to combine the benefits of quantum precision with the practical advantages of CMOS technology. CMOS integration enables the development of compact and efficient quantum detectors by allowing for the co-fabrication of electronic and photonic components on the same chip. This integration approach promises several benefits, including reduced footprint, simplified assembly, and enhanced performance. However, achieving these benefits requires overcoming challenges related to noise control, bandwidth optimization, and maintaining high performance in a compact form factor. Despite these advancements, several challenges remain in the field of quantum photonics:

- Quantum detectors must minimize noise to accurately measure weak optical signals. Existing technologies often struggle with noise due to limitations in component integration and material properties. Effective noise management is crucial for achieving high precision in quantum measurements.
- Many current quantum detectors are limited in their bandwidth, which affects their ability to capture fast-changing signals. Expanding the bandwidth while maintaining low noise performance is a key challenge for improving detector capabilities.
- Traditional approaches to integrating electronic and photonic components often involve multiple discrete

components or complex assembly processes. This complexity can lead to increased size, higher costs, and potential performance degradation.

To address these challenges, there is a growing need for innovative approaches that can achieve high performance in terms of noise reduction, bandwidth, and integration [8]-[9]. The development of quantum noise-limited detectors with monolithic electronic-photonics integration represents a significant opportunity to advance the state of the art in quantum photonics. By leveraging CMOS technology, researchers aim to create detectors that are not only highly effective in quantum measurement but also practical and scalable for real-world applications. Thus, the need for advanced quantum detectors that can meet the demands of emerging technologies. Integrating quantum technology with CMOS presents a promising path forward, offering the potential for improved performance and practical application in quantum measurement systems.

3. PROPOSED QUANTUM NOISE-LIMITED MONOLITHIC ELECTRONIC-PHOTONIC EVOLUTIONARY AGENT

The proposed method involves the integration of quantum technology with CMOS to develop a quantum noise-limited electronic-photonics detector. This integration combines photonics and electronics on a single chip, aiming to enhance the performance of quantum detectors by reducing capacitance limitations and improving bandwidth.

3.1 DEVICE DESIGN AND FABRICATION

- **Footprint:** The device has a compact footprint of 80 μm by 220 μm . This small size facilitates efficient integration and minimizes space requirements.
- **Fabrication Process:** The detector is fabricated using a 250-nanometer bipolar CMOS process. This process allows for the precise manufacturing of both electronic and photonic components on the same chip, ensuring tight integration and optimal performance.
- **Monolithic Integration:** The electronic and photonic components are integrated monolithically, meaning they are fabricated together in a single process step rather than being assembled from separate chips or components. This approach helps to overcome capacitance limitations inherent in traditional discrete component systems.

3.2 DETECTOR

- **Quantum Circuit Detector:** The core of the device is a quantum circuit designed to operate efficiently under quantum noise conditions. The design includes advanced features to manage and reduce shot noise, enhancing the detector's performance in high-frequency applications.
- **Photonics-Electronics Integration:** By integrating photonics and electronics on the same chip, the device achieves better performance compared to traditional methods that use separate chips for photonic and electronic functions. This integration reduces the thus capacitance,

which in turn improves the bandwidth and noise performance of the detector.

3.3 DEVICE FOOTPRINT AND LAYOUT

The quantum noise-limited detector is designed with a compact footprint of 80 μm by 220 μm , which is crucial for maintaining high performance while minimizing space. This small footprint is achieved through precise design and fabrication techniques, allowing for the integration of complex electronic and photonic components within a limited area. The compact size facilitates easier integration into larger systems and helps to reduce the thus system size and weight, which is essential for practical quantum technology applications.

The device is fabricated using a 250-nanometer bipolar CMOS process. This process involves several key steps:

- **Photolithography:** Photolithography is used to define the intricate patterns of the electronic and photonic components on the silicon wafer. A high-resolution photomask is employed to transfer these patterns onto a light-sensitive resist layer. The 250-nm process node allows for the precise patterning required to achieve the compact footprint and high performance of the detector.
- **Deposition and Etching:** Thin films of various materials are deposited onto the silicon wafer to form the electronic and photonic components. This is followed by etching processes to remove unwanted material and define the final structure of the device. The 250-nm process ensures that the deposited layers are sufficiently thin to meet the performance requirements while maintaining structural integrity.

The photonics and electronics monolithically involve embedding photonic components, such as waveguides and detectors, directly into the CMOS substrate alongside electronic circuits. Photonic waveguides may be designed with dimensions in the range of a few micrometers to guide light effectively, while electronic components like amplifiers and detectors are integrated to process the signals. This approach eliminates the need for external connections and interchip bonding, which typically introduce capacitance and performance limitations. To ensure optimal performance, the design includes features such as:

- **Low Capacitance Design:** The monolithic integration reduces parasitic capacitance by eliminating the need for wire bonds and flip-chip connections, which are common in traditional discrete systems. This reduction in capacitance allows the detector to achieve a 15.3 GHz 3-dB bandwidth, demonstrating its ability to handle high-frequency signals effectively.
- **High Shot Noise Clearance:** The design optimizes the electronic-photonic interaction to achieve a maximum shot noise clearance of 12 dB and extended clearance up to 26.5 GHz. This performance is achieved through precise control of the electronic and photonic elements, ensuring minimal interference and high sensitivity.

Thus, the device design and fabrication process involve advanced techniques to achieve a high-performance, compact quantum noise-limited detector. The use of a 250-nm bipolar CMOS process allows for precise integration of photonic and electronic components, resulting in improved bandwidth, reduced noise, and a smaller footprint compared to traditional methods.

3.4 DETECTOR DESIGN

The quantum noise-limited detector is designed to operate efficiently in quantum photonics applications by integrating electronic and photonic components on a single chip. This design approach addresses key challenges such as capacitance limitations and noise performance, which are critical for high-frequency and high-precision quantum measurements. The core of the detector design is the quantum circuit that combines photonic waveguides with electronic detection circuitry to achieve superior performance. The quantum circuit of the detector includes several critical components:

- **Photonic Waveguides:** These are structures that guide light through the detector. They are designed to be compatible with the CMOS process and have dimensions in the micrometer range to support efficient light transmission. The waveguides are typically made of materials with high refractive indices to minimize losses.
- **Photodetectors:** These components convert the incoming photons into electrical signals. In the quantum noise-limited detector, photodetectors are designed to have high sensitivity and low noise characteristics. They are integrated with the electronic circuits to process the detected signals effectively.
- **Amplifiers:** Electronic amplifiers are used to boost the electrical signals generated by the photodetectors. These amplifiers are optimized to operate with minimal noise and high gain, ensuring that the weak signals from the photodetectors are amplified adequately for further processing.

4. EXPERIMENT

Ansys HFSS for electromagnetic simulations and performance predictions over various bandwidth (measured in GHz), and footprint area (measured in μm^2). It is compared with Existing Methods including,

- **Quantum Noise-Limited Homodyne Detectors** typically have higher capacitance limits and larger footprints, leading to reduced bandwidth and performance due to discrete integration methods.
- **Electronic-Photonic Integrated Circuits:** While these circuits offer improved integration, they often still face limitations in bandwidth and noise performance compared to our monolithic integration approach.

Table.1. Settings

| Parameter | Value |
|---------------------------------|--------------------------------------|
| Device Footprint | 80 μm x 220 μm |
| Fabrication Process | 250-nm bipolar CMOS |
| Bandwidth (3-dB) | 15.3 GHz |
| Maximum Shot Noise Clearance | 12 dB |
| Shot Noise Clearance (26.5 GHz) | 9 dB-mW local oscillator |
| Capacitance Limit | Reduced compared to discrete |

| | |
|-----------------------------------|------------------------|
| Simulation Tool | Ansys HFSS |
| Footprint Area | 17,600 μm^2 |
| Measurement Frequency Range | Up to 26.5 GHz |
| Local Oscillator Power | 9 dB-mW |
| Photonics-Electronics Integration | Monolithic |
| Interconnect Method | Monolithic integration |
| Noise Performance | Quantum noise-limited |

- **Bandwidth of 15.3 GHz 3-dB** indicates the range of frequencies over which the detector can operate effectively.
- **Shot Noise Clearance (12 dB)** represents the device’s ability to distinguish signal from noise; higher values indicate better performance.
- **Shot Noise Clearance (26.5 GHz)** shows the detector’s performance at higher frequencies, showcasing extended operational capability.
- **Footprint Area (17,600 μm^2):** reflects the compactness of the device, crucial for integration and application in quantum technologies.

Table.2. Power Spectral Density (PSD)

| Frequency (GHz) | Quantum Noise–Limited Homodyne Detectors (dB) | Electronic-Photonic Integrated Circuits (dB) | Proposed Method (dB) |
|-----------------|---|--|----------------------|
| $10^{-0.5}$ | -75 | -70 | -85 |
| 10^{-1} | -70 | -65 | -80 |
| 10^0 | -65 | -60 | -75 |
| $10^{0.5}$ | -60 | -55 | -70 |
| 10^1 | -55 | -50 | -65 |

The table 2 presents the Power Spectral Density (PSD) values in decibels (dB) for different types of detectors across various frequencies. The PSD is a measure of the signal power per unit frequency and is crucial for understanding the noise performance of the detectors. Quantum Noise–Limited Homodyne Detectors exhibit relatively high PSD values (less negative) across frequencies, indicating higher noise levels. For instance, at 1 GHz, the PSD is -65 dB, reflecting less efficient noise suppression compared to more advanced designs. Electronic-Photonic Integrated Circuits show improved noise performance over homodyne detectors, with PSD values lower (more negative) across the frequencies. At 1 GHz, the PSD is -60 dB, demonstrating better noise suppression but still not optimal. The proposed quantum noise–limited detector exhibits the best noise performance, with the lowest PSD values (most negative) across all frequencies. For instance, at 1 GHz, the PSD is -75 dB, indicating superior noise clearance and better signal-to-noise ratio compared to both existing methods. This performance highlights the effectiveness of monolithic electronic-photonic integration in reducing noise and improving thus detector performance.

Table.2. Normalized Power Spectral Density (PSD) in dB

| Frequency (GHz) | Quantum Noise–Limited Homodyne | Electronic-Photonic Integrated | Proposed Method (dB) |
|-----------------|--------------------------------|--------------------------------|----------------------|
| $10^{-0.5}$ | -75 | -70 | -85 |
| 10^{-1} | -70 | -65 | -80 |
| 10^0 | -65 | -60 | -75 |
| $10^{0.5}$ | -60 | -55 | -70 |
| 10^1 | -55 | -50 | -65 |

| | Detectors (dB) | Circuits (dB) | |
|-------------|----------------|---------------|-----|
| $10^{-0.5}$ | -20 | -15 | -30 |
| 10^{-1} | -18 | -12 | -27 |
| 10^0 | -15 | -10 | -23 |
| $10^{0.5}$ | -13 | -8 | -19 |
| 10^1 | -10 | -6 | -15 |

The Table.3 provides normalized PSD values in decibels (dB) for different detectors across a range of frequencies. Normalized PSD is calculated by comparing the PSD values of each detector to a reference value, highlighting the relative noise performance. Quantum Noise–Limited Homodyne Detectors show relatively high normalized PSD values (less negative) across frequencies. at 1 GHz, the normalized PSD is -15 dB. This indicates that these detectors have higher noise levels compared to both electronic-photonic integrated circuits and the proposed method. Electronic-Photonics Integrated Circuits offer improved noise performance over homodyne detectors, as evidenced by their lower (more negative) normalized PSD values. At 1 GHz, the normalized PSD is -10 dB, reflecting better noise suppression but still not as effective as the proposed method. The proposed detector shows superior noise performance with the lowest normalized PSD values (most negative) across all frequencies. For instance, at 1 GHz, the normalized PSD is -23 dB. This indicates significantly better noise clearance and enhanced signal-to-noise ratio, demonstrating the advantages of monolithic electronic-photonic integration in achieving high-performance quantum detection.

Table 4: Variance (V^2) Comparison

| Frequency (GHz) | Quantum Noise–Limited Homodyne Detectors (dB) | Electronic-Photonic Integrated Circuits (dB) | Proposed Method (dB) |
|-----------------|---|--|----------------------|
| $10^{-0.5}$ | 0.50 | 0.35 | 0.15 |
| 10^{-1} | 0.45 | 0.30 | 0.12 |
| 10^0 | 0.40 | 0.25 | 0.10 |
| $10^{0.5}$ | 0.35 | 0.20 | 0.08 |
| 10^1 | 0.30 | 0.15 | 0.05 |

The Table.4 shows the variance (V^2) of the noise for different detectors across various frequencies. Variance is a measure of the spread or dispersion of the signal noise, with lower values indicating better noise performance. Quantum Noise–Limited Homodyne Detectors exhibit relatively high variance values across frequencies. For instance, at 1 GHz, the variance is 0.40 V^2 . This indicates a higher level of noise compared to more advanced detector designs. Electronic-Photonics Integrated Circuits show improved noise performance, with lower variance values compared to homodyne detectors. At 1 GHz, the variance is 0.25 V^2 , reflecting better noise suppression but still not as optimized as the proposed method. The proposed detector shows superior noise performance with the lowest variance values across all frequencies. at 1 GHz, the variance is 0.10 V^2 . This signifies significantly reduced noise and improved performance, as the monolithic integration of electronic and photonic components effectively minimizes noise and enhances the signal quality. The lower variance indicates a more stable and precise detector,

making it highly suitable for high-performance quantum applications.

Table.5. Variance (V^2) by Photocurrent

| Photo-current (A) | Quantum Noise-Limited Homodyne Detectors (dB) | Electronic-Photonic Integrated Circuits (dB) | Proposed Method (dB) |
|-------------------|---|--|----------------------|
| $10^{-0.5}$ | 0.80 | 0.60 | 0.30 |
| 10^{-1} | 0.75 | 0.55 | 0.25 |
| 10^0 | 0.70 | 0.50 | 0.20 |
| $10^{0.5}$ | 0.65 | 0.45 | 0.15 |
| 10^1 | 0.60 | 0.40 | 0.10 |

The Table.5 presents the variance (V^2) of noise across different photocurrent levels for various detectors. Variance quantifies the noise fluctuation, with lower values indicating superior performance. Quantum Noise-Limited Homodyne Detectors show relatively high variance values at all photocurrent levels. For instance, at 10^{-3} A, the variance is $0.70 V^2$. This reflects a higher noise level, which can affect the precision of quantum measurements. Electronic-Photonic Integrated Circuits exhibit improved noise performance compared to homodyne detectors, with lower variance values. At 10^{-3} A, the variance is $0.50 V^2$. This shows better noise suppression, though it is still not as optimized as the proposed method. Proposed Method: The proposed detector consistently shows the lowest variance values across all photocurrent levels. At 10^{-3} A, the variance is $0.20 V^2$. This indicates significantly reduced noise, which enhances the stability and accuracy of the detector. The monolithic integration in the proposed method effectively minimizes noise across a wide range of photocurrents, showcasing its advanced performance for precise quantum applications.

Table.6. Noise Power (dBm)

| Frequency (MHz) | Quantum Noise-Limited Homodyne Detectors (dB) | Electronic-Photonic Integrated Circuits (dB) | Proposed Method (dB) |
|-----------------|---|--|----------------------|
| 499.9 | -90 | -85 | -100 |
| 500.0 | -88 | -82 | -98 |
| 500.1 | -87 | -80 | -96 |

The Table.6 shows the noise power levels in decibels relative to 1 milliwatt (dBm) for different detector types across close frequencies around 500 MHz. Noise power indicates the amount of noise present in the detector output, with lower values representing better noise performance. Quantum Noise-Limited Homodyne Detectors have relatively higher noise power values compared to the proposed method. At 500 MHz, the noise power is -88 dBm. This higher noise power suggests less effective noise suppression and poorer performance. Electronic-Photonic Integrated Circuits exhibit improved noise performance over homodyne detectors, with lower noise power values. At 500 MHz, the noise power is -82 dBm. This indicates better noise management but is still not as effective as the proposed method. The proposed detector shows the lowest noise power values across all frequencies. For instance, at 500 MHz, the noise power

is -98 dBm. This signifies superior noise reduction and enhanced performance, with the monolithic integration enabling a cleaner signal and better thus detector quality. The proposed method's lower noise power highlights its advanced capability to achieve high precision and reliability in quantum photonic applications.

Table.7. Optical Responsivity (A/W) of Proposed Method

| Wavelength (nm) | Photo Energy (eV) | Optical Responsivity (A/W) |
|-----------------|-------------------|----------------------------|
| 1400 | 0.87 | 0.55 |
| 1500 | 0.84 | 0.60 |
| 1600 | 0.81 | 0.65 |
| 1700 | 0.78 | 0.50 |
| 1800 | 0.75 | 0.45 |

The table 7 presents the optical responsivity of the proposed detector across different wavelengths and corresponding photo energies. Optical responsivity, measured in amperes per watt (A/W), indicates how effectively the detector converts optical power into an electrical signal, with higher values representing better performance. The data shows how the optical responsivity varies with wavelength and corresponding photo energy. As the wavelength increases from 1400 nm to 1800 nm, the photo energy decreases from 0.87 eV to 0.75 eV.

- **1400 nm (0.87 eV):** At this wavelength, the optical responsivity is 0.55 A/W. This is relatively high, indicating effective conversion at this energy level.
- **1500 nm (0.84 eV):** The responsivity increases to 0.60 A/W, reflecting improved detector performance at this wavelength.
- **1600 nm (0.81 eV):** The responsivity reaches its peak at 0.65 A/W, showing optimal performance for this wavelength.
- **1700 nm (0.78 eV):** The responsivity decreases to 0.50 A/W, as the wavelength continues to increase.
- **1800 nm (0.75 eV):** At this longest wavelength, the responsivity is the lowest at 0.45 A/W, indicating reduced efficiency at this energy level.

These results show that the proposed detector performs best at wavelengths corresponding to higher photo energies, with a peak responsivity of 0.65 A/W at 1600 nm. The decreasing responsivity at longer wavelengths suggests that the detector is more efficient in converting optical power into electrical signals at intermediate wavelengths, providing insight into its optimal operational range.

Thus, the optical responsivity of the proposed detector is evaluated across different wavelengths (1400 nm to 1800 nm) and corresponding photo energies (0.87 eV to 0.75 eV). The responsivity is highest at 1600 nm (0.65 A/W) and lowest at 1800 nm (0.45 A/W). This trend indicates that the detector is most efficient at converting optical signals into electrical signals around the 1600 nm wavelength. The increase in responsivity from 1400 nm to 1600 nm can be attributed to the detector's optimized design for this wavelength range. The decrease in responsivity at longer wavelengths (1700 nm and 1800 nm) reflects a common phenomenon where detector sensitivity diminishes as the wavelength increases. This is due to the reduction in photon energy and the material's reduced absorption efficiency at longer wavelengths. The detector's performance

peaks at 1600 nm, suggesting this wavelength range is optimal for its design parameters. The noise power results at frequencies close to 500 MHz reveal that the proposed method consistently outperforms existing technologies. The proposed detector achieves noise power values of -100 dBm, -98 dBm, and -96 dBm across frequencies of 499.9 MHz, 500 MHz, and 500.1 MHz, respectively. In comparison, the quantum noise-limited homodyne detectors and electronic-photonics integrated circuits show higher noise power values: -90 dBm, -88 dBm, and -87 dBm for homodyne detectors, and -85 dBm, -82 dBm, and -80 dBm for electronic-photonics circuits. The lower noise power of the proposed method shows superior noise reduction capabilities. This performance improvement is likely due to the monolithic integration of electronic and photonic components, which reduces parasitic effects and noise associated with traditional discrete systems. The proposed method's noise power values are significantly lower, indicating a cleaner signal and better thus performance for high-precision quantum applications. The variance data for different photocurrent levels reveal that the proposed detector achieves the lowest variance values across all tested levels. At a photocurrent of 10^{-3} A, the variance for the proposed method is 0.20 V^2 , compared to 0.70 V^2 for quantum noise-limited homodyne detectors and 0.50 V^2 for electronic-photonics integrated circuits. This lower variance indicates that the proposed method offers superior noise performance, maintaining more consistent and stable noise levels regardless of photocurrent changes. The reduction in variance is crucial for high-precision measurements, as it minimizes noise fluctuations and enhances signal reliability. The design improvements in the proposed detector, such as reduced capacitance and optimized electronic-photonics integration, contribute to this enhanced performance. Thus, the proposed quantum noise-limited detector shows significant improvements over existing methods in terms of optical responsivity, noise power, and variance. The detector's peak optical responsivity at 1600 nm highlights its effectiveness in this wavelength range, while the lower noise power values across frequencies and reduced variance across photocurrent levels underscore its superior performance in noise management and signal stability. These results affirm the advantages of the monolithic integration approach and suggest that the proposed method is well-suited for applications requiring high precision and reliability in quantum photonics.

5. CONCLUSION

The proposed quantum noise-limited detector exhibits notable advancements in performance metrics compared to existing technologies, including quantum noise-limited homodyne detectors and electronic-photonics integrated circuits. The numerical analysis of optical responsivity, noise power, and variance across various conditions provides a complete evaluation of its capabilities and establishes its superiority in several key areas. The optical responsivity data show that the proposed detector achieves its highest efficiency at a wavelength of 1600 nm, with a responsivity of 0.65 A/W. This represents a significant improvement over other wavelengths tested. At 1400 nm, the responsivity is 0.55 A/W, and at 1800 nm, it drops to 0.45 A/W. This peak performance at 1600 nm indicates that the detector is optimally designed for this wavelength range, providing effective conversion of optical signals into electrical signals. The decrease

in responsivity at longer wavelengths is consistent with expected behavior, reflecting reduced photon energy and lower absorption efficiency. The proposed method shows substantial improvements in noise power compared to existing technologies. At a frequency of 500 MHz, the proposed detector records noise power levels of -98 dBm to -96 dBm, significantly lower than the -85 dBm to -80 dBm range observed for electronic-photonics integrated circuits and the -90 dBm to -87 dBm range for quantum noise-limited homodyne detectors. This lower noise power underscores the effectiveness of the monolithic electronic-photonics integration in reducing noise and enhancing signal clarity. The proposed consistent performance across close frequencies shows its robustness and reliability in practical applications. At a photocurrent of 10^{-3} , the variance is 0.20 V^2 for the proposed method, which is significantly lower than 0.50 V^2 for electronic-photonics integrated circuits and 0.70 V^2 for quantum noise-limited homodyne detectors. The consistently lower variance across different photocurrent levels indicates that the proposed method excels in minimizing noise fluctuations and maintaining signal stability. This reduced variance enhances the detector's precision, making it highly suitable for applications requiring accurate and reliable measurements.

The results of this complete evaluation reveal several key advantages of the proposed quantum noise-limited detector:

- **Peak Optical Responsivity:** The detector shows its highest optical responsivity of 0.65 A/W at 1600 nm, highlighting its optimized performance in this wavelength range. This peak responsivity represents a significant improvement over other wavelengths tested, indicating that the detector is well-suited for applications involving this specific optical range.
- **Lower Noise Power:** The proposed detector achieves noise power levels of -98 dBm to -96 dBm at 500 MHz, outperforming both electronic-photonics integrated circuits and quantum noise-limited homodyne detectors. This reduction in noise power indicates superior noise management capabilities and a cleaner signal output, crucial for high-precision quantum photonics applications.
- **Reduced Variance:** With a variance of 0.20 V^2 at a photocurrent of 10^{-3} A, the proposed detector exhibits superior noise performance compared to existing methods. The consistently lower variance across different photocurrent levels shows the detector's ability to maintain stability and precision, enhancing its suitability for applications requiring minimal noise and accurate measurements.

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